

Aircraft Design I

Loads

Flight (Loads) envelope

Aircraft loads

- What is the source of loads?
- How to compute this ?
- What values are critical?
- What we have to do, when critical case is difficult to compute?

Load factor

$$n = \frac{P_z}{Q} = \frac{L}{W}$$

Load factor what is the value?

straight level flight

$$P_z = Q, \text{ thus } n=1$$

turn

$$n = \sqrt{\left(\frac{\Omega V}{g}\right)^2 + 1}$$

regular turn

$$n = \sqrt{\frac{q \pi A e}{W/S} \left(\left(\frac{T}{W} \right)_{\max} - \frac{q C_{D0}}{W/S} \right)}$$

max. lift coefficient $C_{L,\max}$

$$n = \frac{\rho V^2 S C_{L,\max}}{2W}$$

What is in the regulations?

There are two groups of loads:

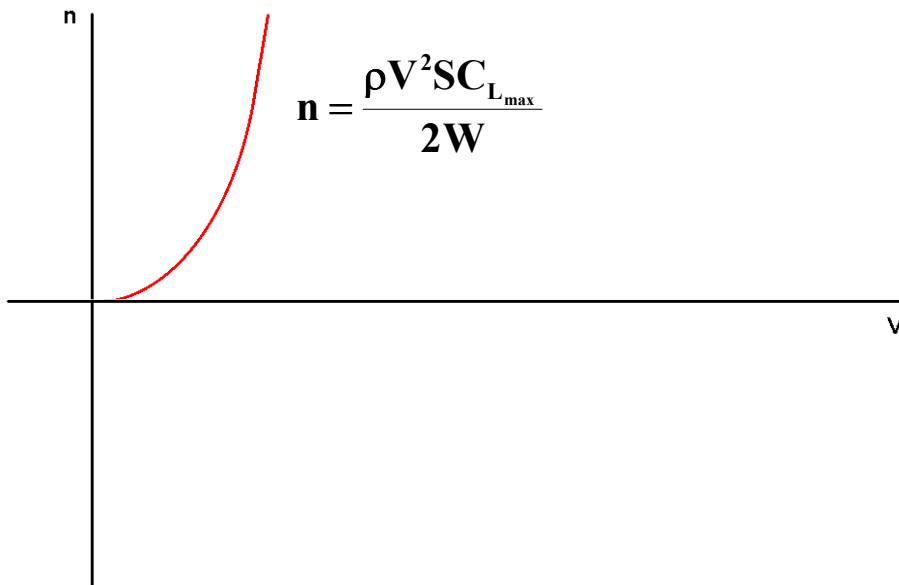
- control,
- gust.

Regulations require to compute the flight envelope $n(V)$

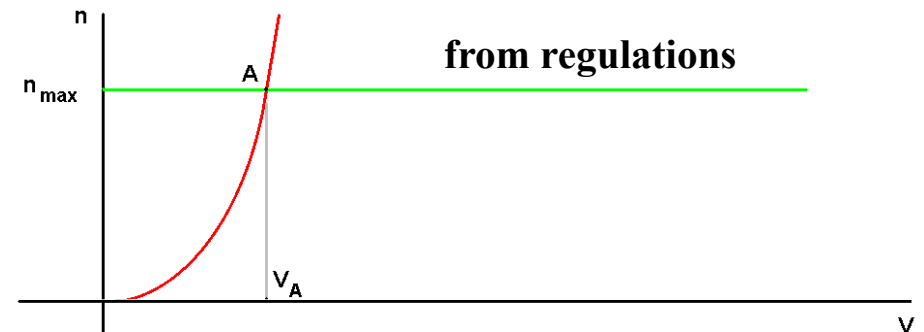
Control loads



Control loads



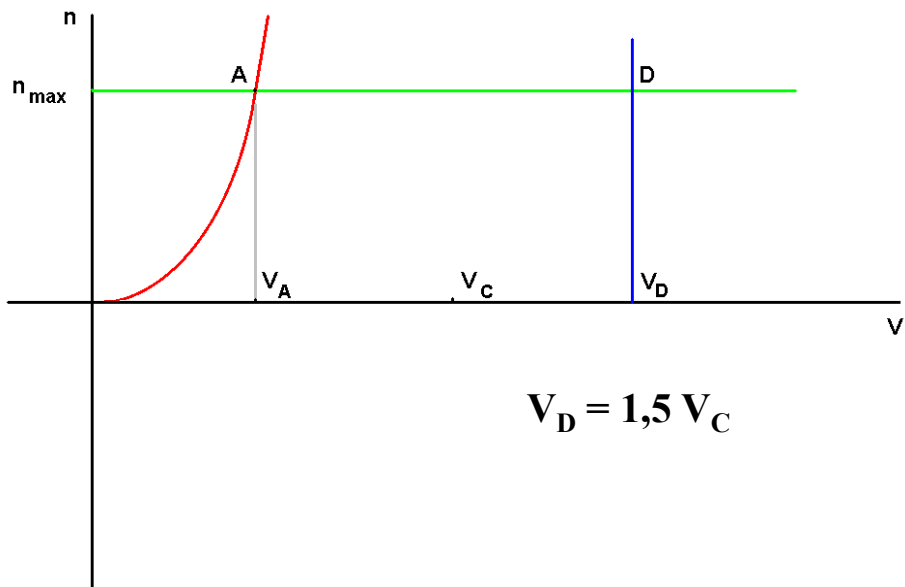
Control loads



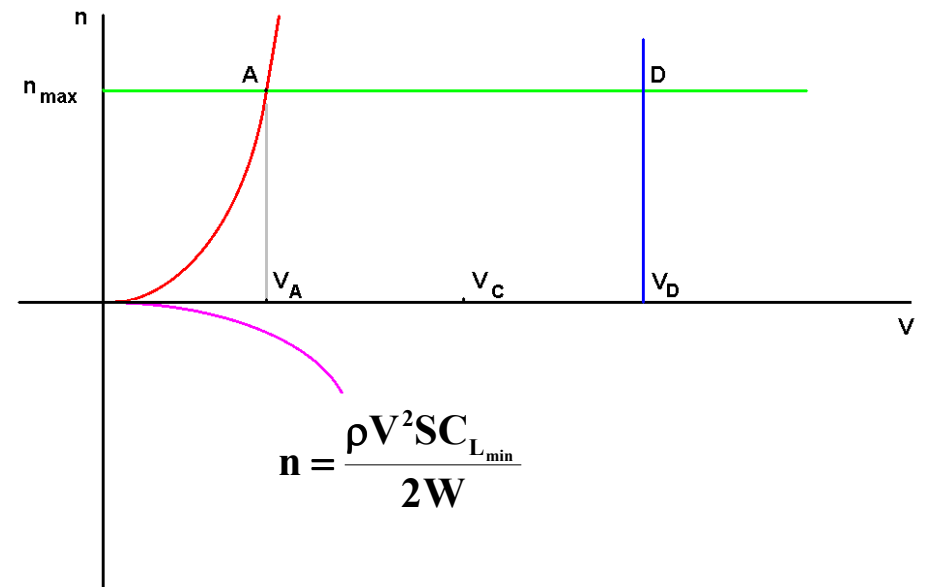
Standard Airworthiness Certification Regulations

**FAR 23
FAR 25
JAR 22
JAR-VLA**

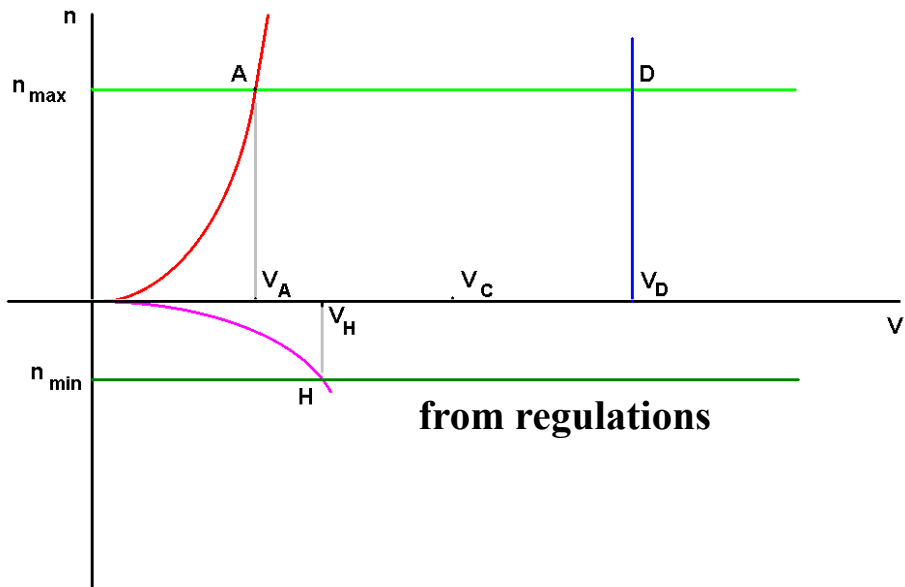
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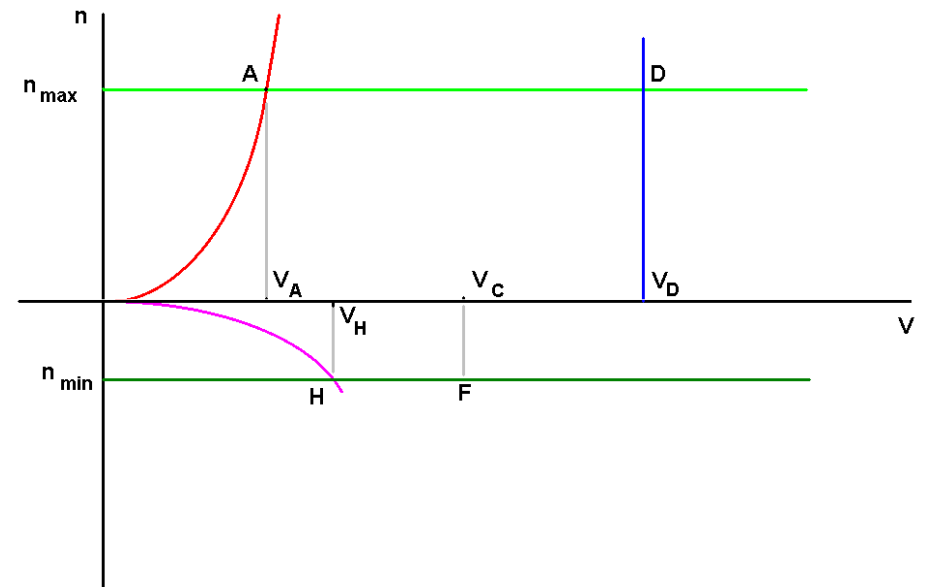
Control loads



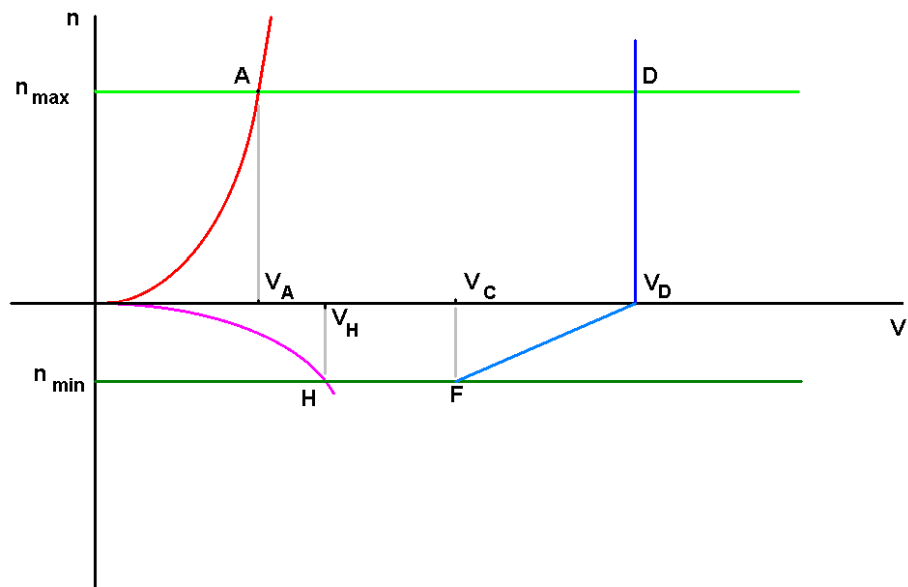
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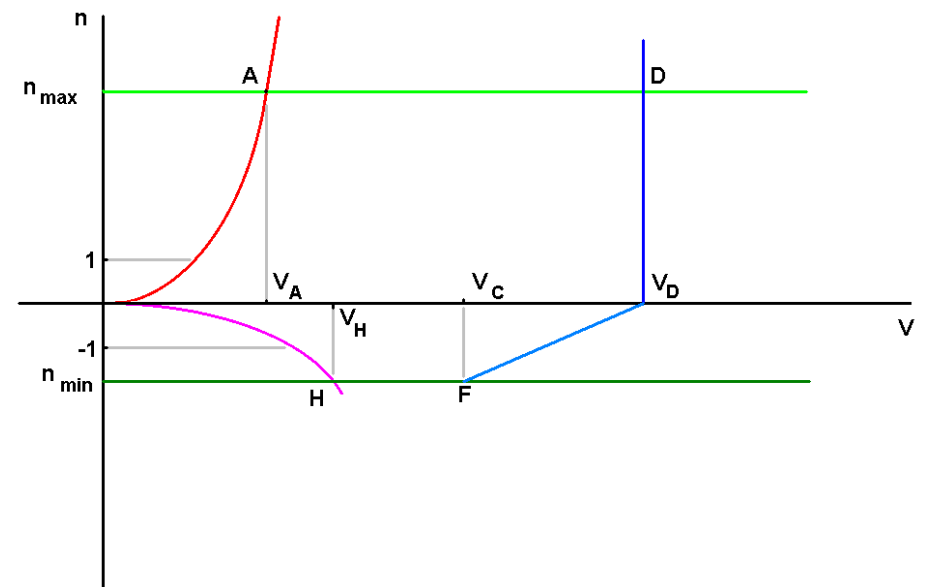
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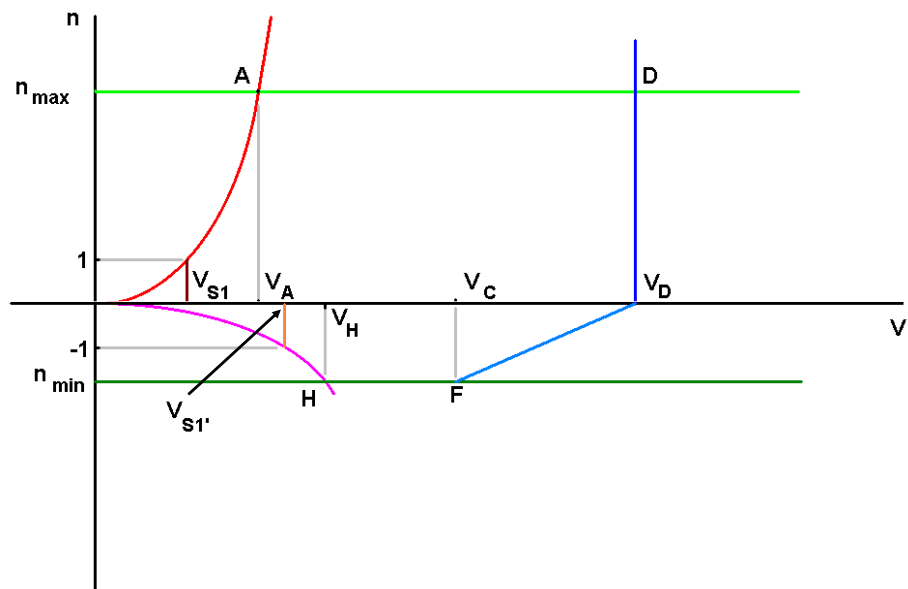
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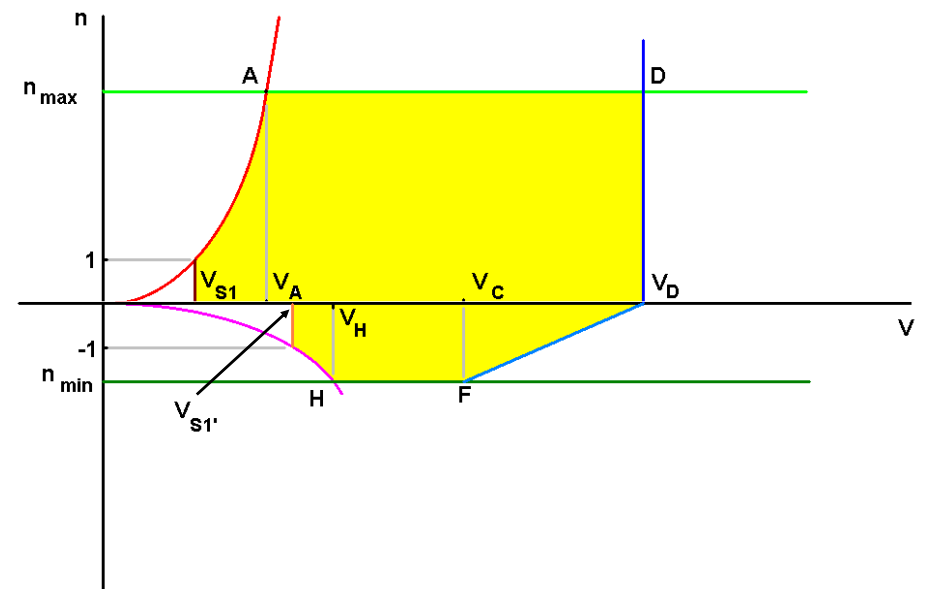
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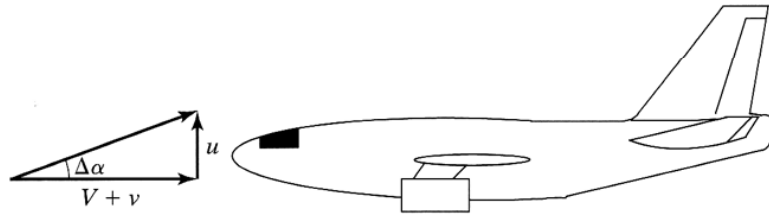
Control loads



Control loads



Gust loads

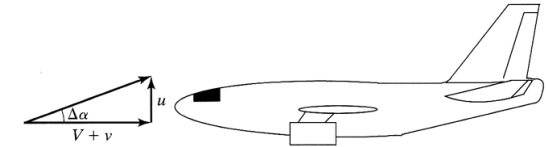


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u i v are small comparing to V

$$V+v \simeq V.$$

$$\Delta\alpha = \tan^{-1} \frac{u}{V} \simeq \frac{u}{V}.$$



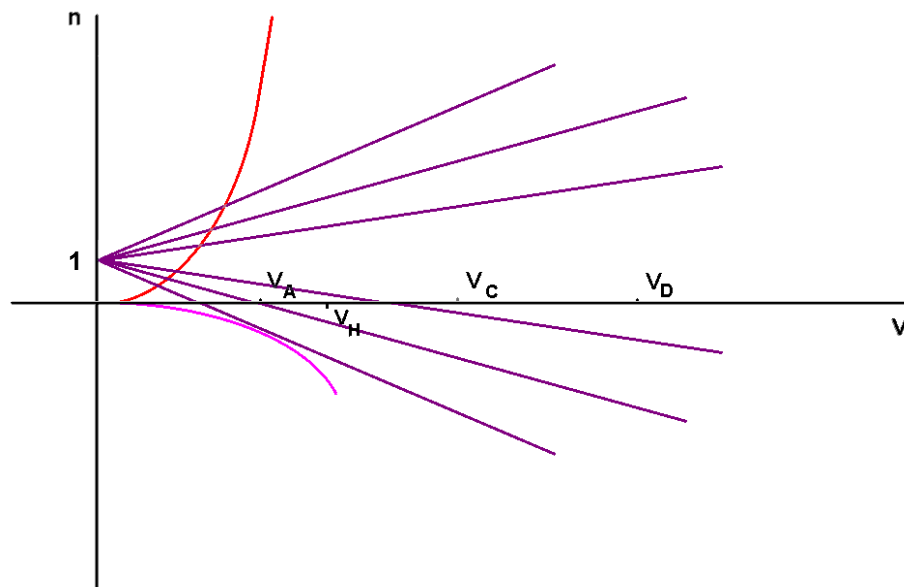
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$$\Delta L = \frac{1}{2} \rho V^2 S C_{L_\alpha} \Delta\alpha = \frac{1}{2} \rho V S C_{L_\alpha} u.$$

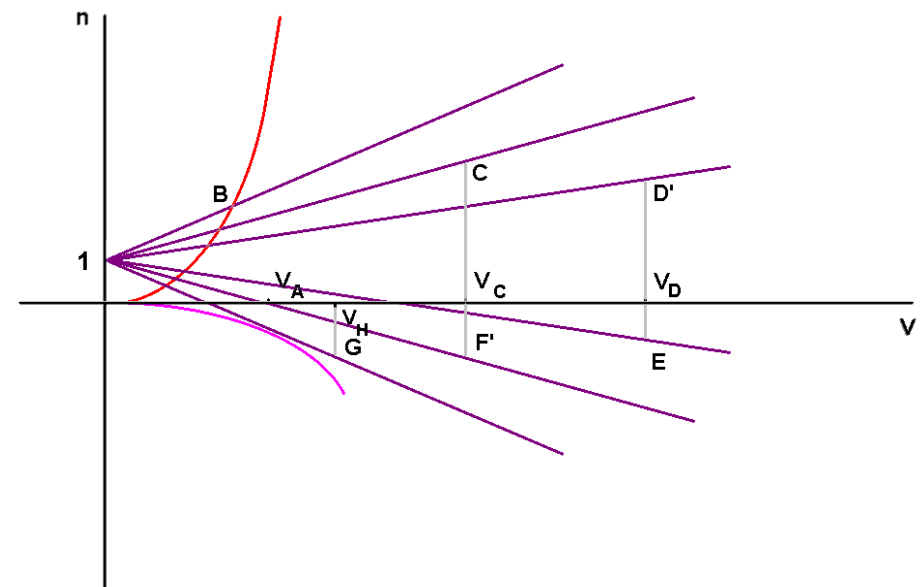
$$\Delta n = \frac{\rho u V C_{L_\alpha}}{2W/S}$$

$$n_{\text{peak}} = n + \Delta n.$$

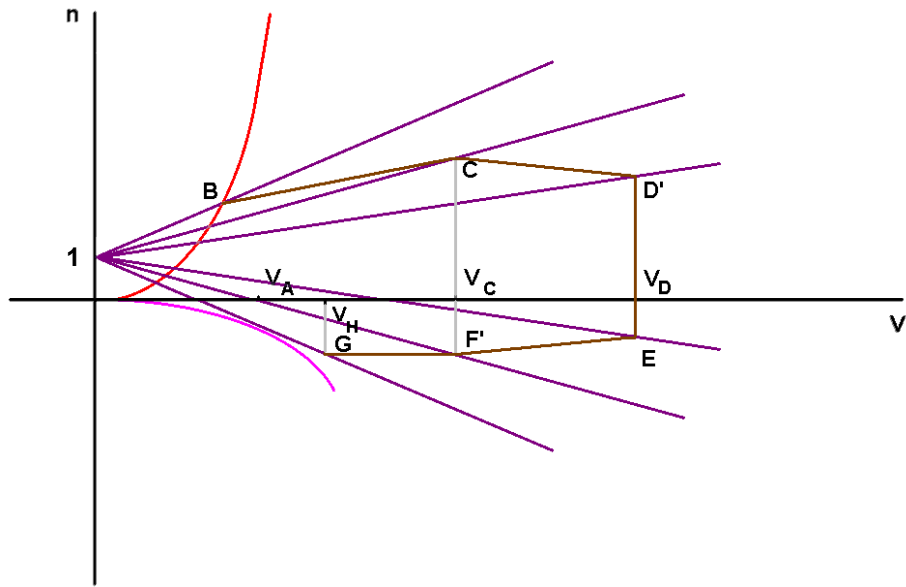
Gust loads



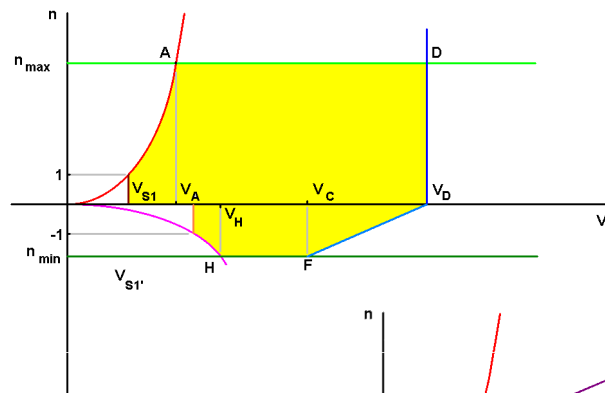
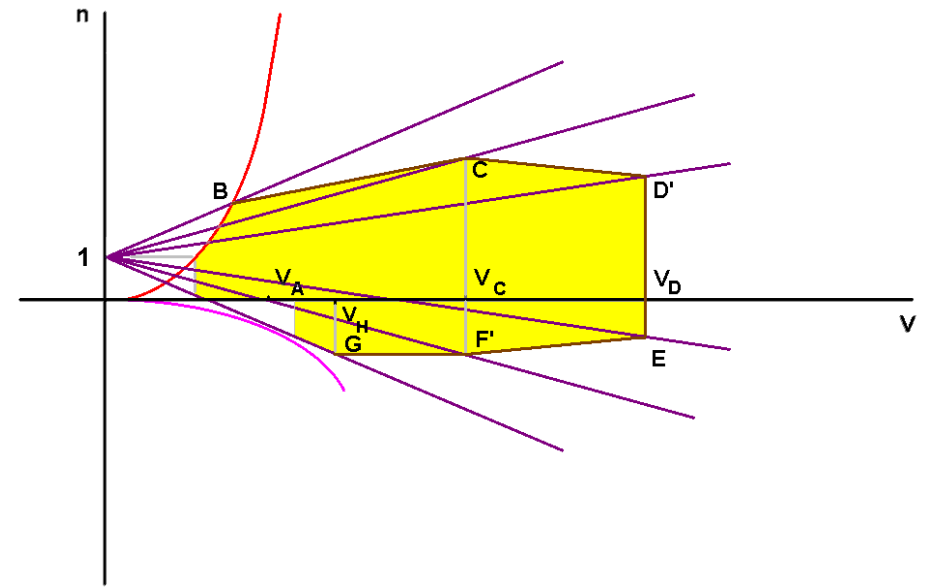
Gust loads



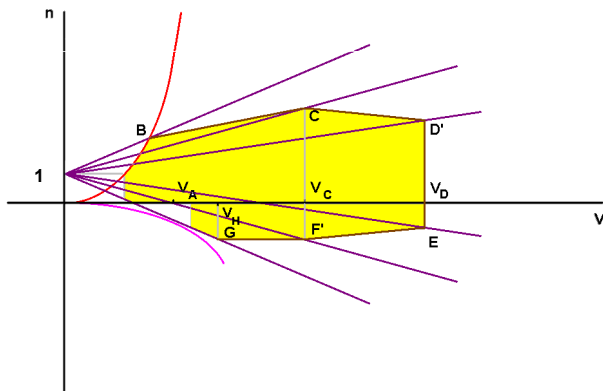
Gust loads



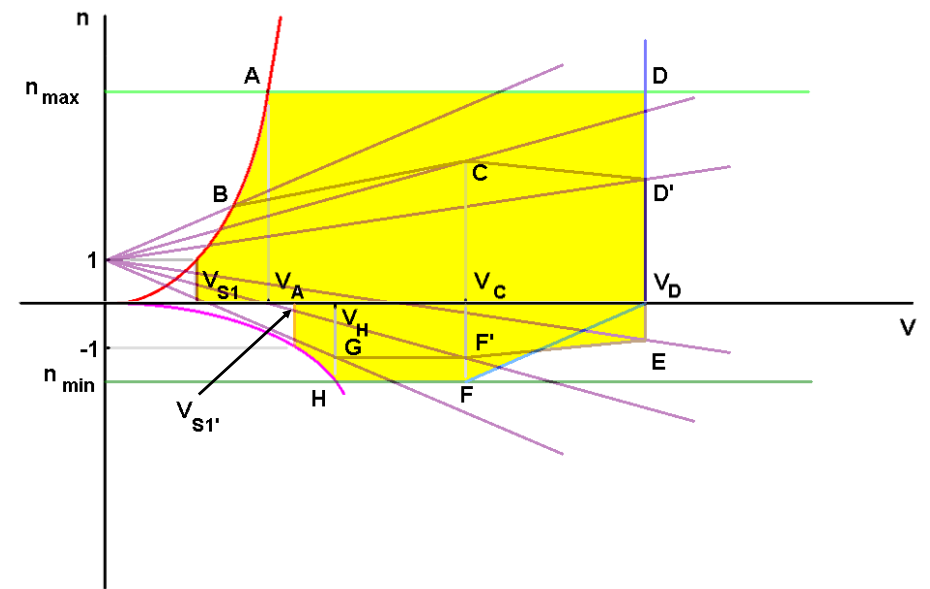
Gust loads

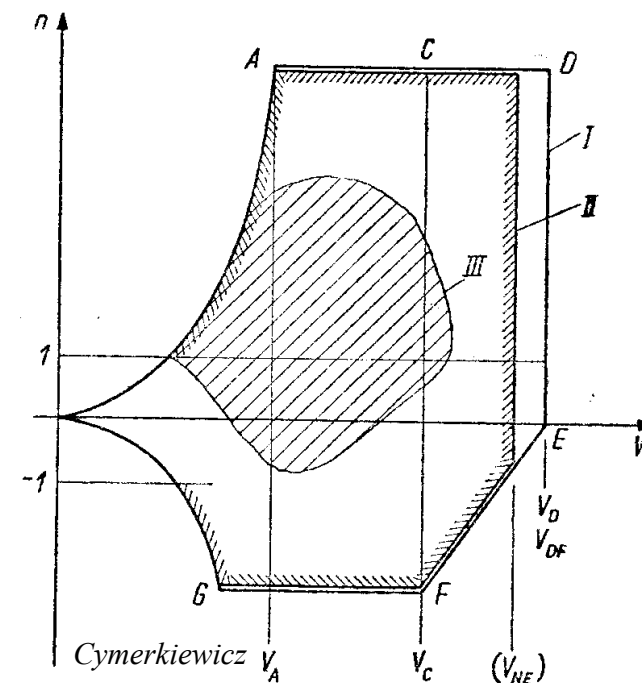
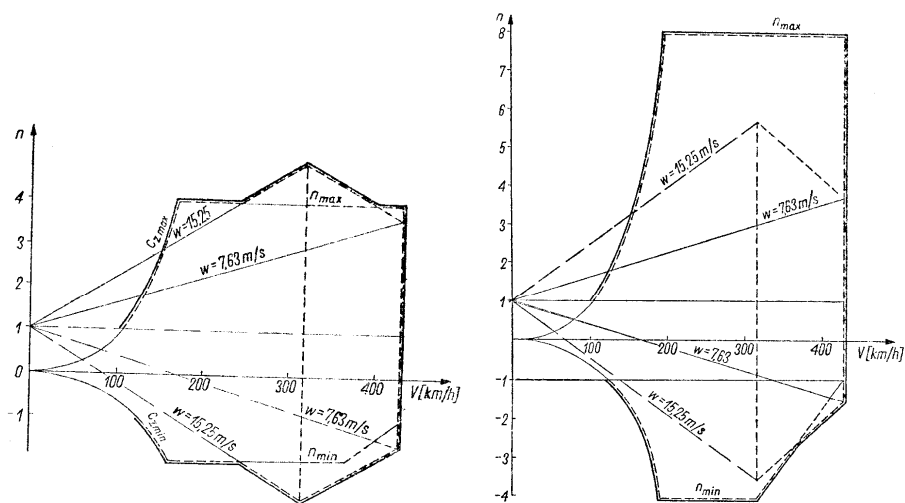


What now?



Envelope





European Aviation Safety Agency

CS-23

Amendment 2 (Corrigendum)
28 September 2010

Appendix 2: Consensus

- **CS 23.303 Factor of safety**
Unless otherwise provided, a factor of safety of
1,5 must be used

Lift distribution on the wing

How compute the real wing load
having $n(V)$

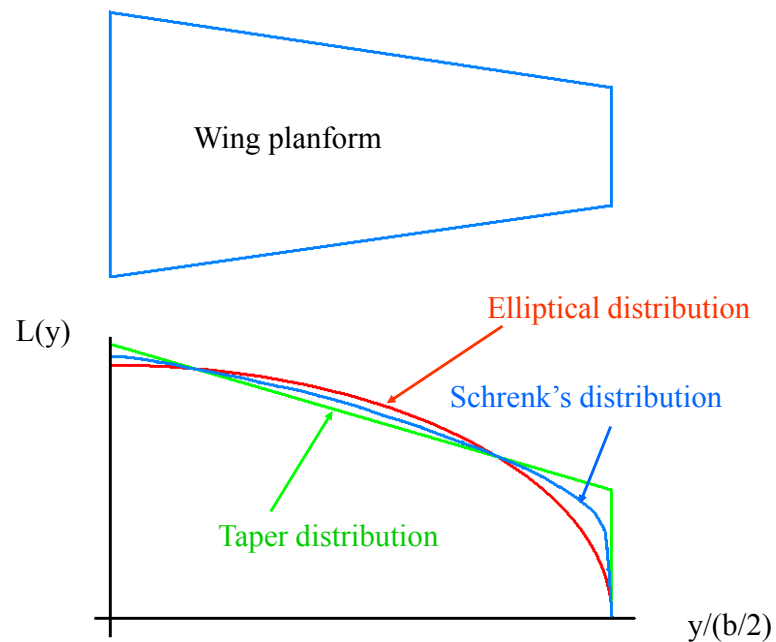
For elliptical wing

Chord vs. wingspan

$$c(y) = \frac{4S}{\pi b} \sqrt{1 - \left(\frac{2y}{b}\right)^2}$$

Lift distribution

$$L^E(y) = \frac{4L}{\pi b} \sqrt{1 - \left(\frac{2y}{b}\right)^2}$$



For taper wing

Chord vs. wingspan:

$$c(y) = c_r \left[1 - \frac{2y}{b} (1 - \lambda) \right]$$

Non-real taper lift
distribution:

$$L^T(y) = L_r \left[1 - \frac{2y}{b} (1 - \lambda) \right]$$

Total lift force:

$$L = \int_{-b/2}^{b/2} L(y) dy = 2L_r \int_0^{b/2} \left[1 - \frac{2y}{b} (1 - \lambda) \right] dy$$

For taper wing

Total lift force:
$$L = \frac{L_r b(1 + \lambda)}{2}$$

Root „Lift force”
$$L_r = \frac{2L}{b(1 + \lambda)}$$

Non-real taper lift distribution :
$$L^T(y) = \frac{2L}{b(1 + \lambda)} \left[1 - \frac{2y}{b}(1 - \lambda) \right]$$

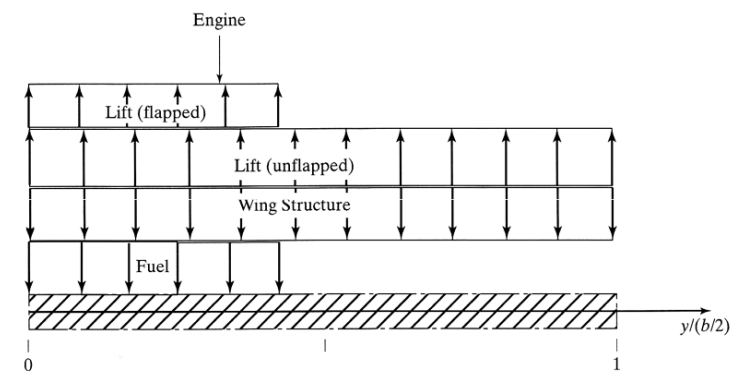
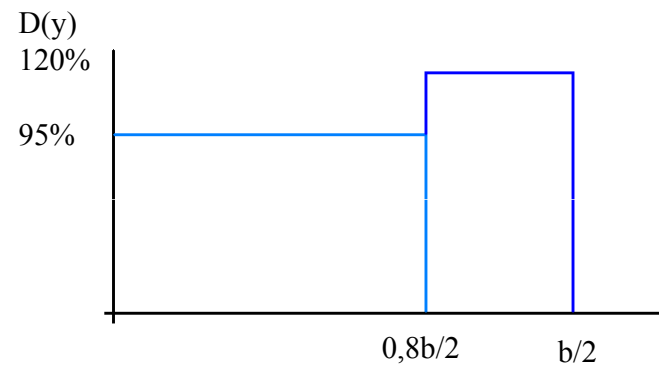
For taper wing

Schrenk's lift distribution:

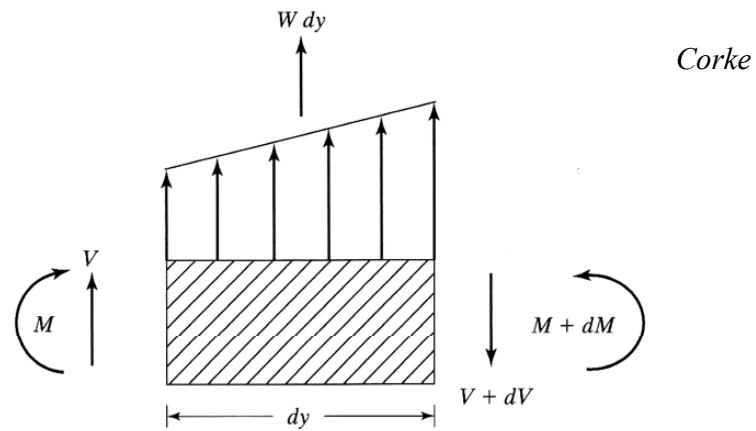
$$\bar{L}(y) = \frac{1}{2} \left[L^T(y) + L^E(y) \right]$$

$$L^E(y) = \frac{4L}{\pi b} \sqrt{1 - \left(\frac{2y}{b} \right)^2}$$

$$L^T(y) = \frac{2L}{b(1 + \lambda)} \left[1 - \frac{2y}{b}(1 - \lambda) \right]$$



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Unit load $\rightarrow W = \frac{dV}{dy}$ \leftarrow shearing force $\rightarrow V = \frac{dM}{dy}$ \leftarrow bending moment

$$V = \int W dy$$

$$M = \int V dy.$$

or after approximation $V = \sum_i^N W_i \Delta y$

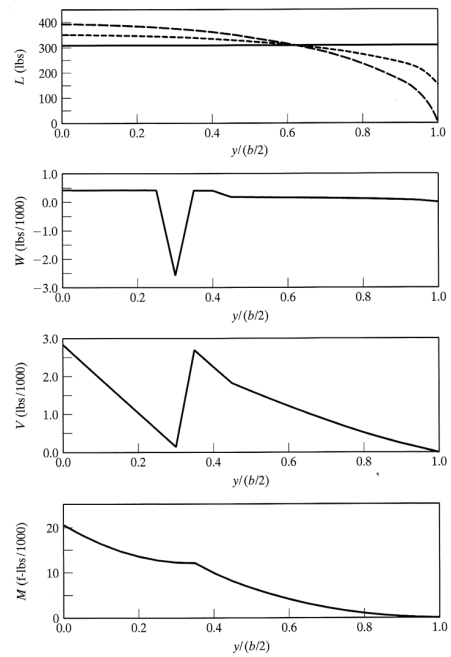
$$M = \sum_i^N V_i \Delta y,$$

Shearing force distribution

$$\begin{aligned} V_1 &= 0; \\ V_2 &= W_1 + W_2; \\ V_3 &= W_1 + W_2 + W_3 = V_2 + W_3; \\ V_4 &= V_3 + W_4; \\ &\vdots \\ V_N &= V_{N-1} + W_N. \end{aligned}$$

Bending moment distribution

$$\begin{aligned} M_1 &= 0; \\ M_2 &= V_1 + \Delta y V_2; \\ M_3 &= V_1 + \Delta y V_2 + \Delta y V_3 = M_2 + \Delta y V_3; \\ M_4 &= M_3 + \Delta y V_4; \\ &\vdots \\ M_N &= M_{N-1} + \Delta y V_N. \end{aligned}$$



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